

Research into Low-Frequency Surge Underpredictions of Floating Offshore Wind Turbines

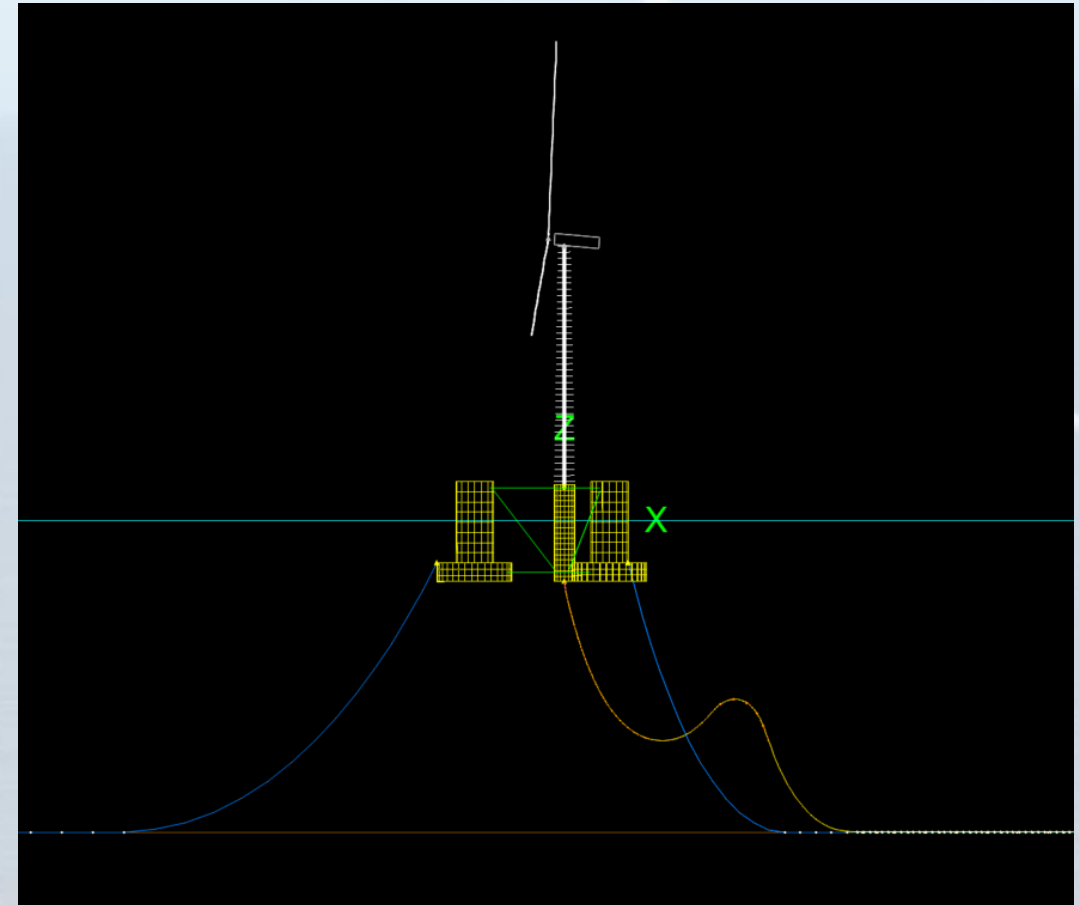
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Project Overview

- Flexible Coupled Multi-Body Dynamic Research of Floating Offshore Wind Turbines (FOWT).

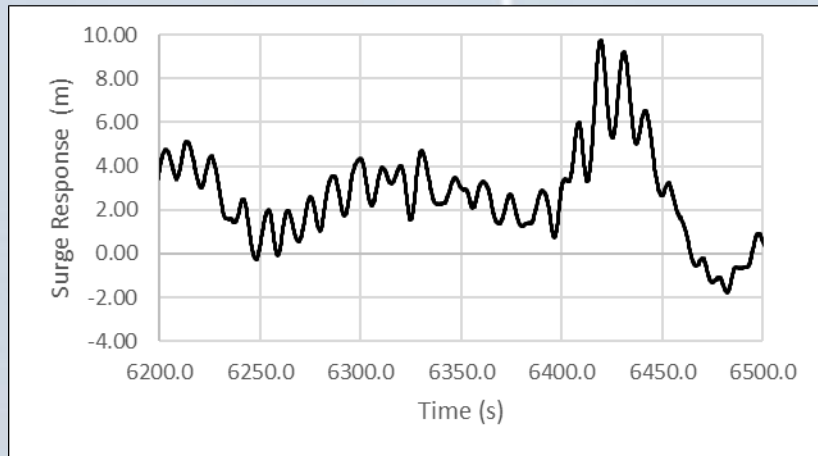
Aims:

- To improve vessel response prediction.
- To create more cost-effective and efficient FOWTs.

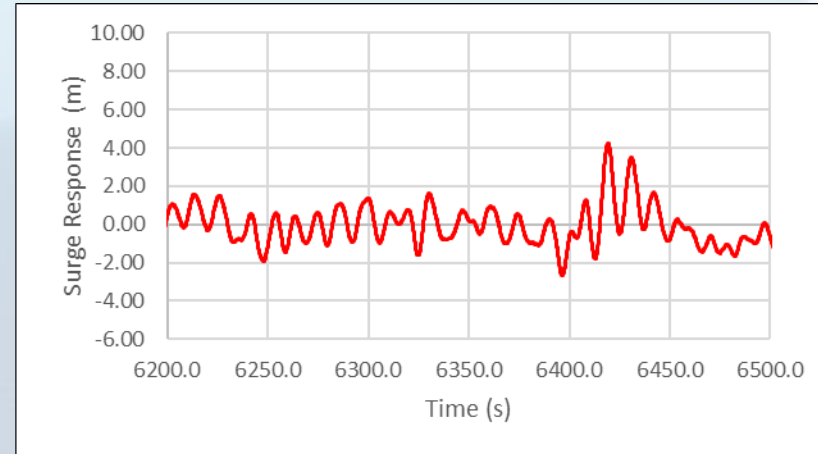


FOWT model in Orcaflex

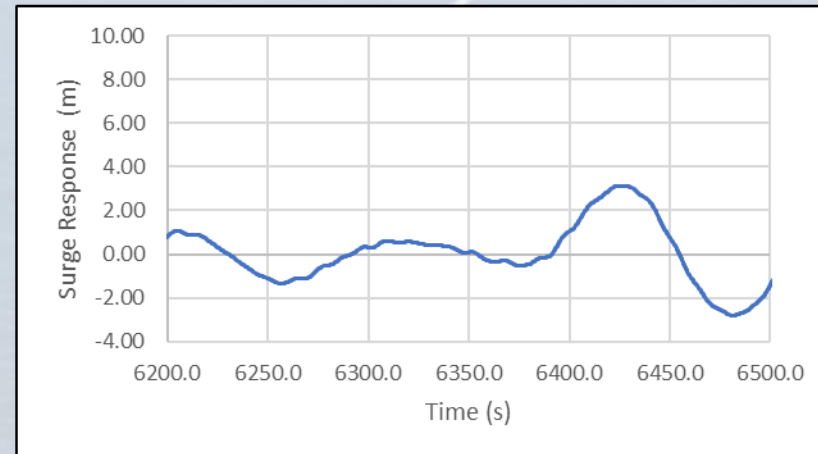
Low-frequency Motion Response



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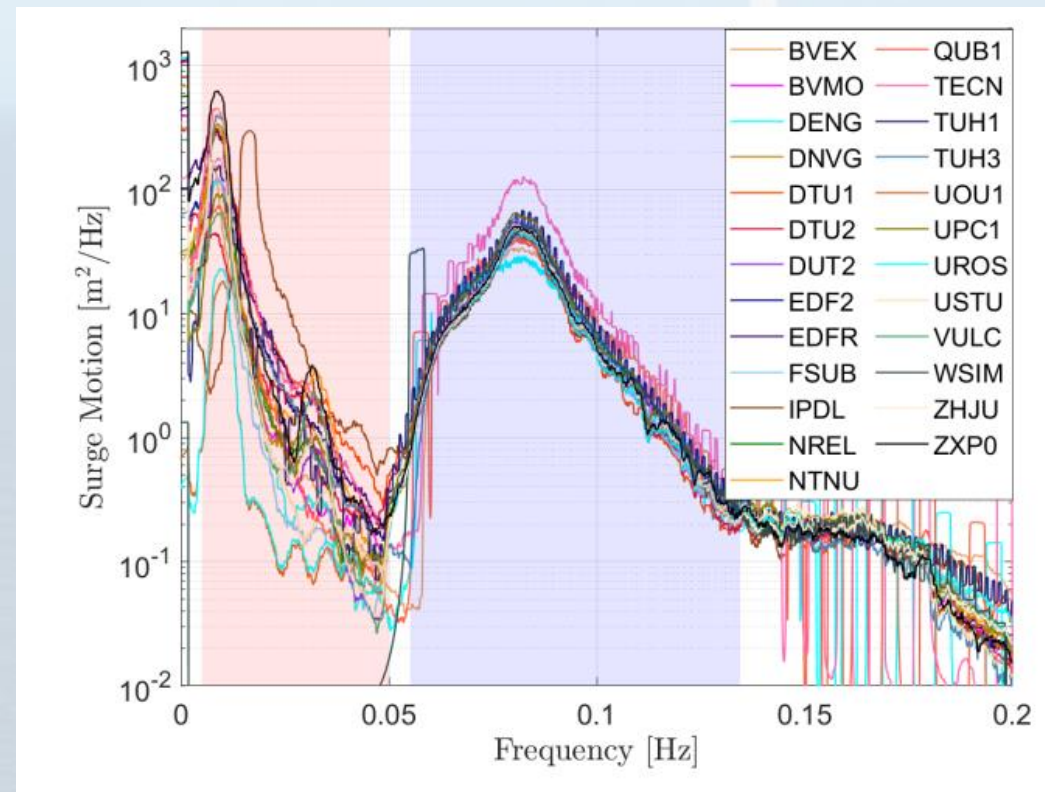


Wave-frequency response

Low-frequency response

Low-Frequency Surge Underprediction

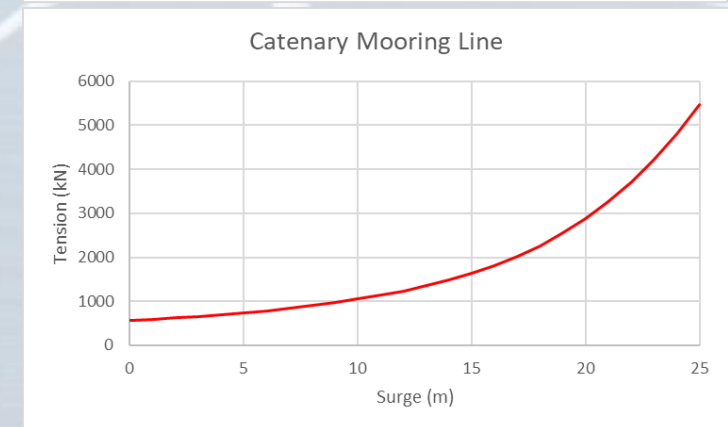
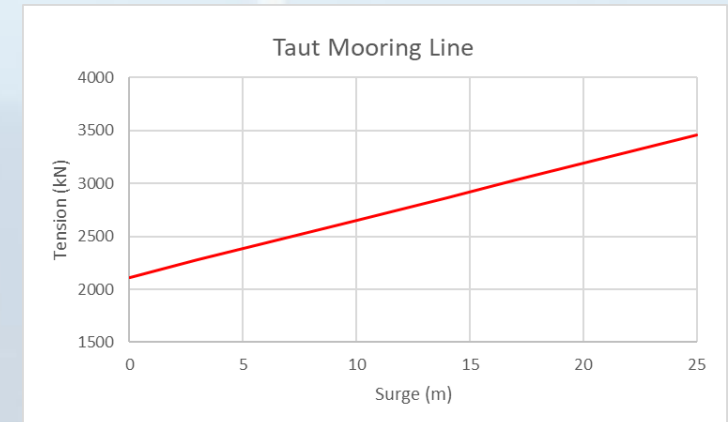
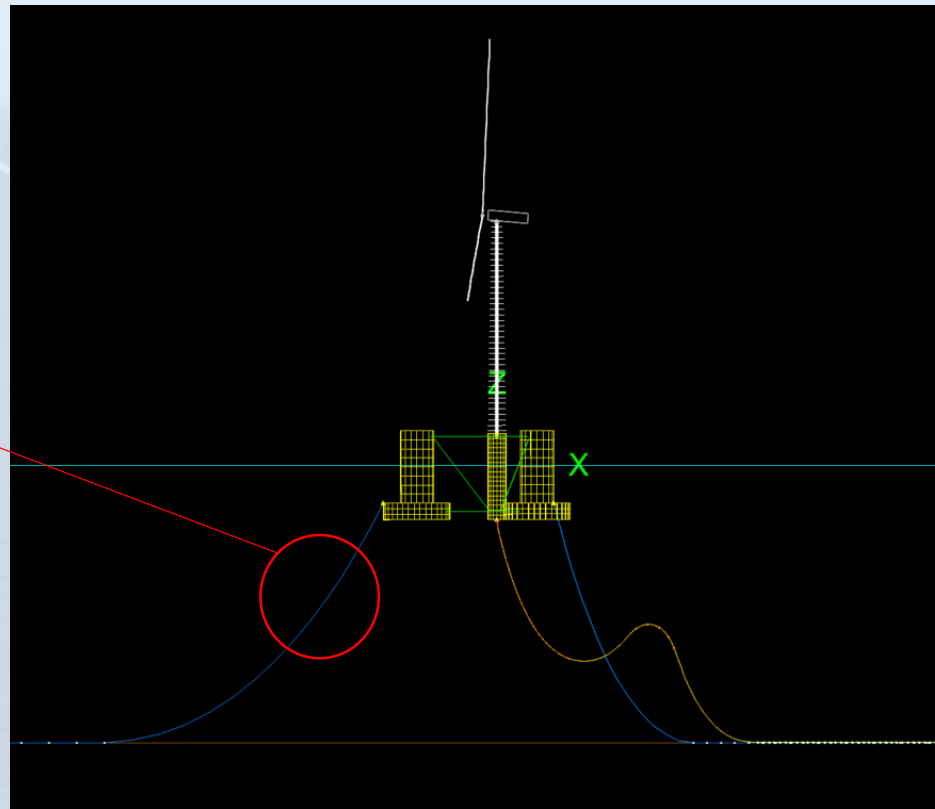
- Previous studies have found an underprediction of up to 20% in low-frequency loads and motions.



Surge power spectral density from [1]

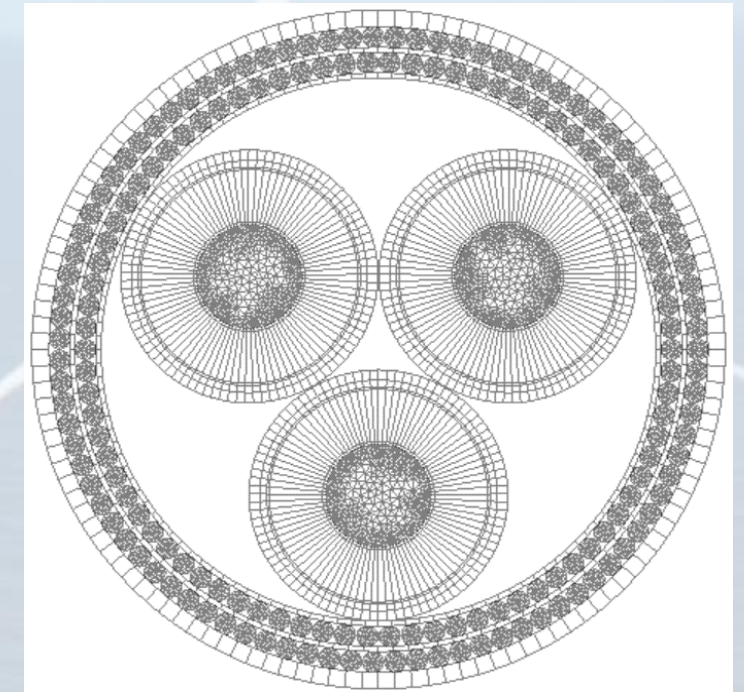
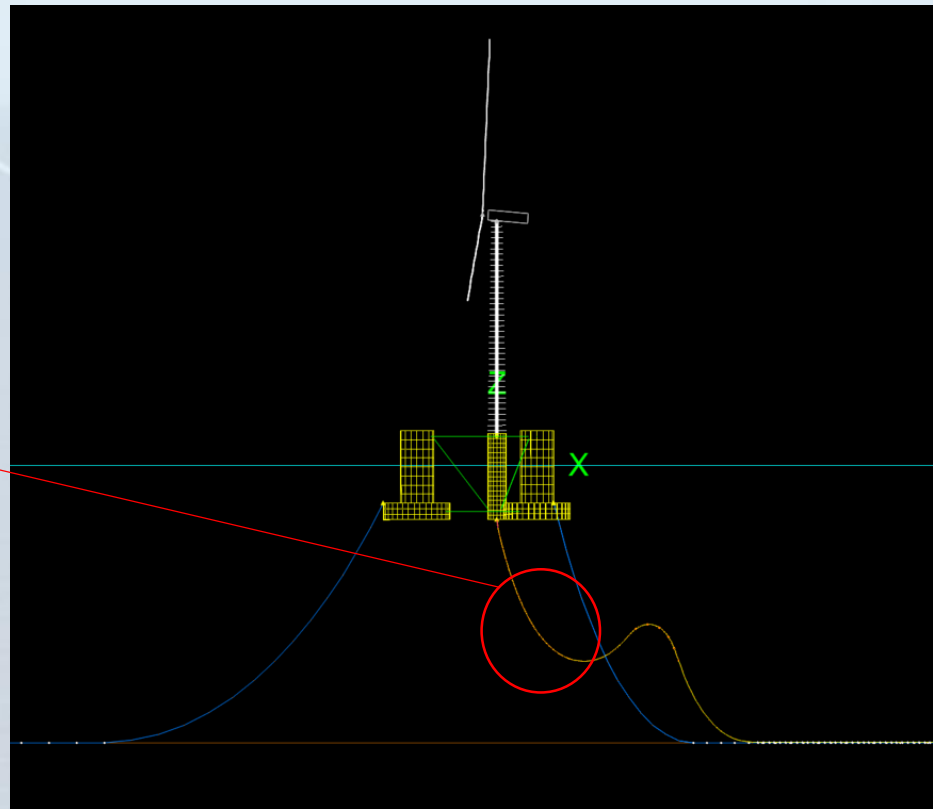
Underprediction Consequences

Potential for mooring line tension to exceed design limit. Catastrophic failure in multiple offshore drilling platforms [2].



Underprediction Consequences

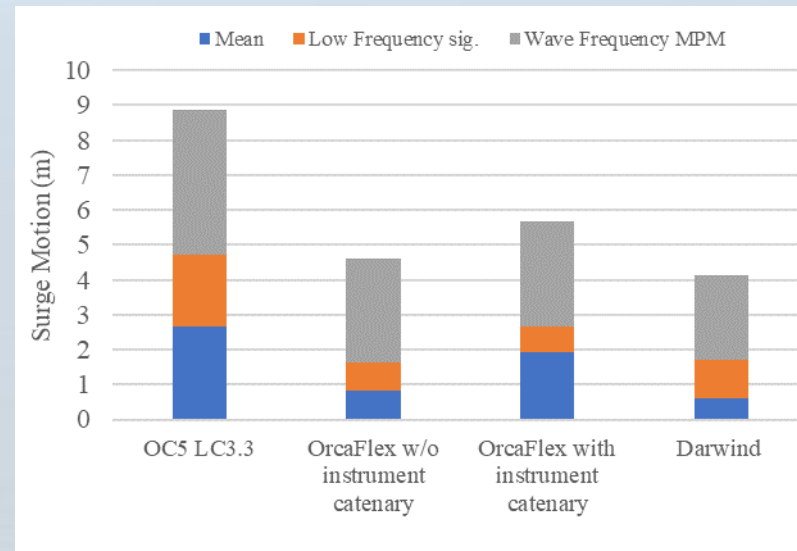
Fatigue damage sustained by power cables from motion can increase by up to 13% [3].



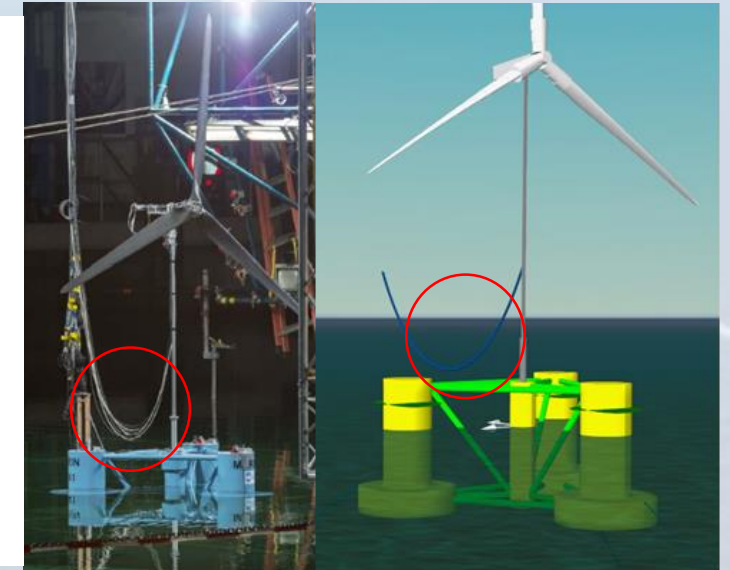
Cable cross-section modelled in UFLEX

Low-Frequency Surge Underprediction

- Initial Testing Clearly shows the underprediction in low-frequency response shown in orange.
- Initial simulations and decay tests showed that the instrument catenary had a significant effect on the mean offset.



Initial model testing

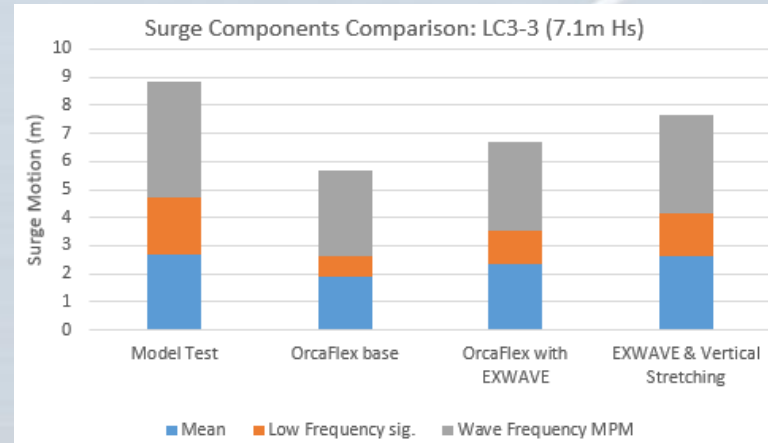
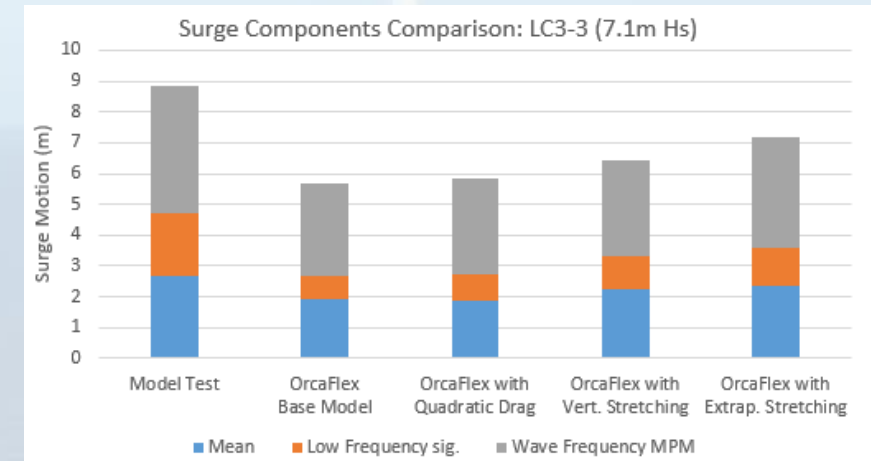


OC4 DeepCWind Experiment [4] vs OrcaFlex simulation model

Low-Frequency Corrections

- When using wave stretching techniques, which extend wave velocity above the water line, the prediction is closer to that of the model test [5].
- This is further improved when the quadratic transfer functions (QTFs) are corrected using the EXWAVE correction.

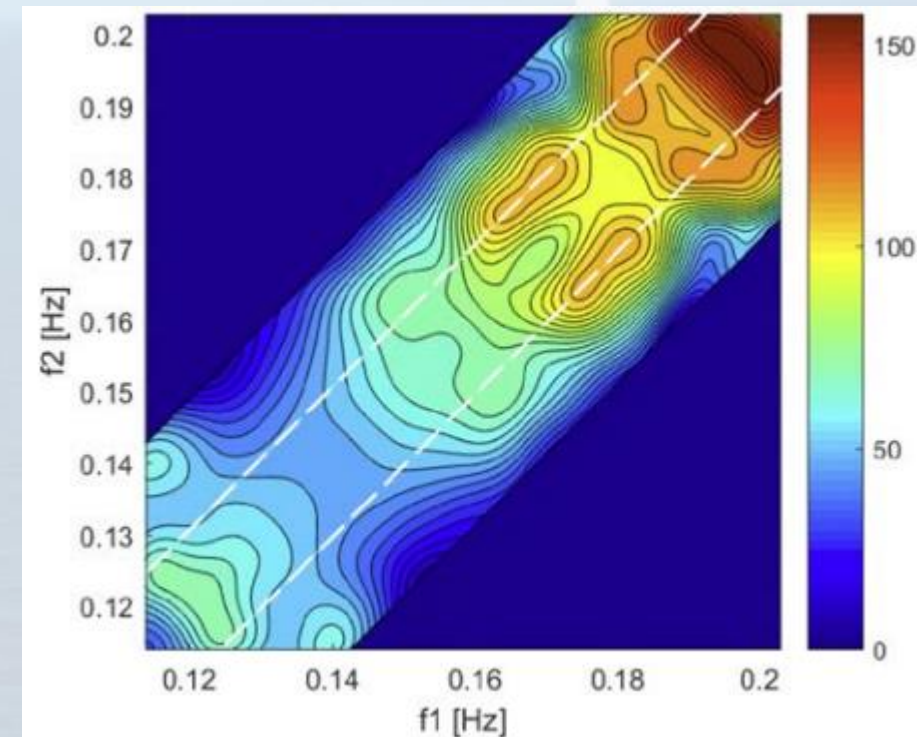
Effects on response when using various wave stretching techniques



Effects on response when incorporating the EXWAVE correction

Quadratic Transfer Functions (QTFs)

- Used to calculate the low-frequency forces generated from wave component pairs of frequencies f_1 and f_2 .
- Normal generated through diffraction analysis software.



Quadratic transfer function (kNm^{-2}) from [6]

Empirical QTF



Cross-Bi-Spectral Analysis

$$H = FFT(h)$$

$$G^{(2)} = FFT(g)$$

$$S_{hh}(f) = (1/T) \langle |H(f)|^2 \rangle$$

$$S_{hhg}(f_m, f_n) = (1/T) \langle H^*(f_m)H(f_n)G^{(2)}(f_m - f_n) \rangle$$

$$H^{(2)}(f_m, f_n) = S_{hhg}(f_m, f_n) / S_{hh}(f_m)S_{hh}(f_n)$$

Where:

$$H^{(2)}(f_m, f_n) = QTF$$

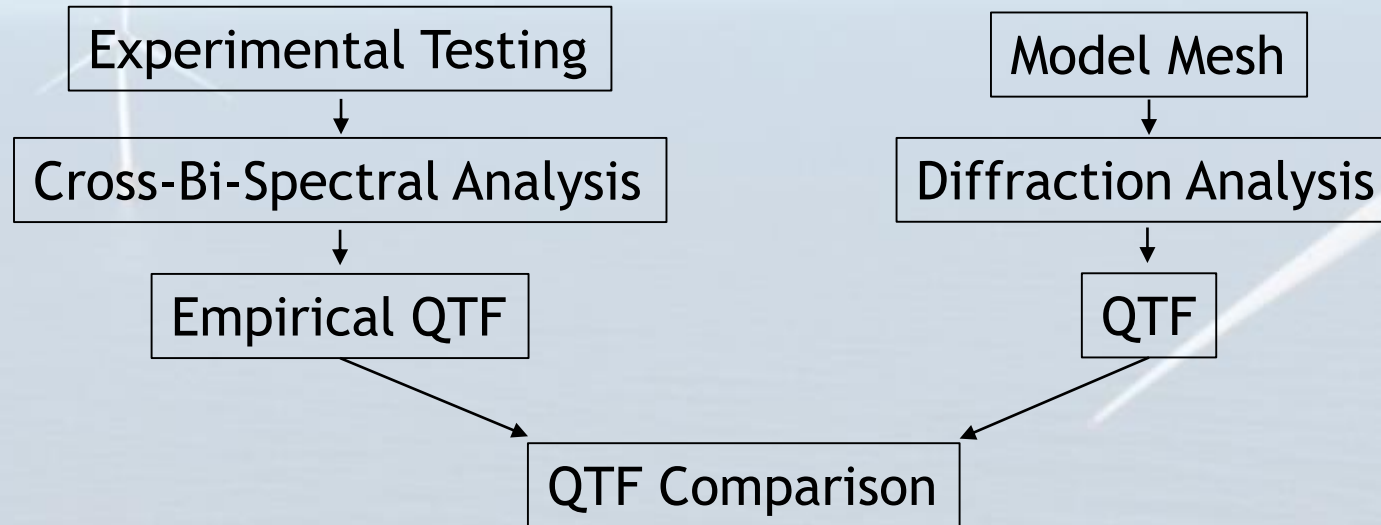
S_{hh} = two-sided autospectrum of h

S_{hhg} = cross-bi-spectrum

$\langle \rangle$ = statistical average


* = complex conjugate

Quadratic Transfer Functions (QTFs)



Summary

- Low-frequency forces and motions are currently underpredicted by up to 20% in floating offshore wind turbines which could lead to damage to mooring lines and power cables.
- Using various correction factors reduces this but not completely.
- Current work involves using experimental data to calculate the quadratic transfer function to compare to that calculated by diffraction analysis.



Thank you for Listening
Any Questions?

Empirical QTF



From Experiment: H (wave elevation) and X (surge motion)

$$\ddot{x}_{LF}(t) + \zeta \dot{x}_{LF}(t) + K(t) = \frac{1}{m} g(t)$$

\ddot{x}_{LF} = Low-frequency surge motion

ζ = Linearised damping coefficient

K = Mooring restoring force

m = Vessel mass

g = 2nd order difference frequency wave exciting force

Cross-Bi-Spectral Analysis

$$H = FFT(h)$$

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$$S_{hh}(f) = (1/T) \langle |H(f)|^2 \rangle$$

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